



Preface

Content

Interactive design aids for masonry elements in accordance to BS EN 1996

Guidelines of use

After installing a free trial or demo version the interactive templates will be available free of charge. The only requirement is a registration at www.VCmaster.com.

The examples provided have been created using VCmaster. All annotated and illustrated design aids can be used as a basis to create own templates. In order to do this a full version of VCmaster is necessary.

All templates are linked to various databases by TAB()- or SEL() functions. For instructional purposes these links are displayed in this document, but can also be hidden when printing.

What is VCmaster?

VCmaster is a software application for technical documentation specifically designed for engineers. The unique software concept integrates all structural design and CAD software. Universal interfaces guarantee data transfer, so that the output of all programs can be transposed.

Beside its functions for documentation, VCmaster offers an intuitive concept enabling engineers to carry out calculations. The input of mathematic formulas can be executed in natural notation directly in the document itself. The software significantly supports the reuse of structural calculations and documents. VCmaster simplifies modifications and adjustments and automates standard tasks. Collaboration with work-groups or with other offices and clients is uncomplicated as well. As a result, processing time and costs can be considerably reduced.

System Requirements

VCmaster 2016 or newer

Development and Copyrights

Developed in Germany
VCmaster is a registered trademark
© Veit Christoph GmbH 1995-2016
www.VCmaster.com

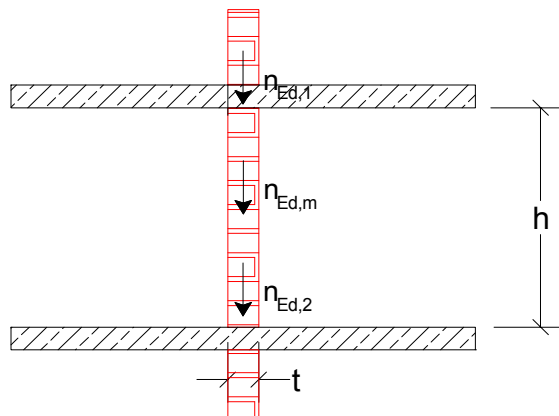


Contents

Preface	1
Contents	2
Chapter 1: Examples	3
Vertical load capacity of an intermediate wall	3
Load capacity of an external wall (roof)	5
Load capacity of an external wall	8
Chapter 2: Simplified method	11
Vertical load capacity of an intermediate wall	11
Load capacity of an external wall (roof)	13
Load capacity of an external wall	15
Chapter 3: Concentrated loads	17
Lintel bearing	17
Beam bearing on a wall	19
Chapter 4: Formulas for moments	21
Content: Formulae for the moment of a wall panel	21
Formula for the moment of a wall panel (A)	22
Formula for the moment of a wall panel (C)	23
Formula for the moment of a wall panel (E)	24
Formula for the moment of a wall panel (B)	25
Formula for the moment of a wall panel (D)	26
Formula for the moment of a wall panel (F)	27
Chapter 5: Material	28
Compressive strength of masonry	28

Chapter 1: Examples

Vertical load capacity of an intermediate wall



Data given

Effective thickness t_{ef} =	140.00 mm
Clear height h =	2800.00 mm
Effective height reduction factor ρ =	0.75
Total load for ULS N_{Ed} =	125.00 kN/m

Material properties

Control class	=	2
Category	=	I
γ_m	=	2.70

Reduction factor

Effective height h_{ef} =	$\rho * h = 0.75 * 2800.00$	=	2100.00 mm
Slenderness λ =	$\frac{h_{ef}}{t_{ef}} = \frac{2100.00}{140.00}$	=	15.00 < 27
Factor Φ_A =		=	1.00
Factor Φ_s =	$A_1 * e^{(-0,5 * u^2)}$	=	0.747

Material selected

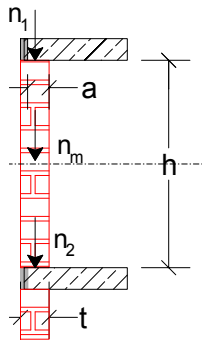
Structural units	=	Aggregate concrete
Classification group	=	1
Type of mortar	=	general
Mean compressive strength of masonry unit f_b =	7.10 N/mm ²	
Compressive strength of mortar f_m =	6.00 N/mm ²	



Shape factor			
Height of unit h		=	215.00 mm
Width of unit w =			140.00 mm
δ		=	1.300
f_b =	$\delta * f_b = 1.300 * 7.10$	=	9.23 N/mm ²
f_k =	$K * f_b^\alpha * f_m^\beta = 0.55 * 9.23^{0.70} * 6.00^{0.30}$	=	4.46 N/mm ²
f_d =	$\frac{f_k}{\gamma_m} = \frac{4.46}{2.70}$	=	1.65
N_{Rd} =	$\frac{f_d * t_{ef} * 10^3 * \Phi_A * \Phi_s}{10^3} = \frac{1.65 * 140.00 * 10^3 * 1.00 * 0.747}{10^3}$	=	172.56 kN
$\frac{N_{Ed}}{N_{Rd}}$ =	$\frac{125.00}{172.56}$	=	0.72 ≤ 1



Load capacity of an external wall (roof)



Data given

Effective thickness t_{ef} =	140.00 mm
Clear height h =	2800.00 mm
Effective height reduction factor ρ =	0.75
Total load for ULS N_{Ed} =	150.00 kN/m

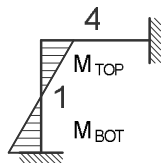
Material properties

Control class	=	2
Category	=	I
γ_m	=	2.70

Slenderness

Effective height $h_{ef} = \rho * h = 0.75 * 2800.00$	=	2100.00 mm
Slenderness $\lambda = \frac{h_{ef}}{t_{ef}} = \frac{2100.00}{140.00}$	=	15.00 < 27
Factor $\Phi_A =$		1.00

Moments at the top and at the bottom



Data given for the wall

Clear height $h_1 =$	h	=	2800.00 mm
Depth of wall $h =$	t_{ef}	=	140.00 mm
Strength $f_k =$			4.05 N/mm ²
$E_1 =$	$f_k * 10^3$	=	4050.00 N/mm ²
$I_1 =$	$\frac{1000 * h^3}{12} = \frac{1000 * 140.00^3}{12}$	=	228.67 * 10 ⁶ mm ⁴



Data given for the roof

Load $w_4 = 8.10$ kN/m
 Span of roof $L_4 = 6500.00$ mm
 Roof or floor depth $h = 200.00$ mm

Concrete grade = C30/37

$E_4 = 33000.00$ N/mm²

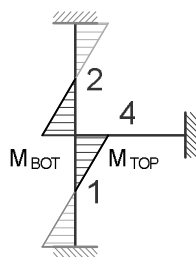
$$I_4 = \frac{850 \cdot h^3}{12} = \frac{850 \cdot 200.00^3}{12} = 566.67 \cdot 10^6 \text{ mm}^4$$

Moment at the top

$$\eta = \text{MAX} \left(1 - \frac{\frac{E_4 \cdot I_4}{L_4}}{4 \cdot \frac{E_1 \cdot I_1}{h_1}}; 0.5 \right) = 0.50$$

$$M_{\text{top}} = \eta \cdot \frac{\frac{E_1 \cdot I_1}{h_1}}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_4 \cdot I_4}{L_4}} \cdot \frac{-1 \cdot w_4 \cdot L_4^2}{12} = -1.47 \text{ kNm/m}$$

Moment at the bottom



Data given for the floor

Load $w_4 = 10.00$ kN/m

$$\eta = \text{MAX} \left(1 - \frac{\frac{E_4 \cdot I_4}{L_4}}{4 \cdot \left(\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} \right)}; 0.5 \right) = 0.50$$

$$M_{\text{bot}} = \eta \cdot \frac{\frac{E_1 \cdot I_1}{h_1}}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} + \frac{E_4 \cdot I_4}{L_4}} \cdot \frac{w_4 \cdot L_4^2}{12} = 1.65 \text{ kNm/m}$$

$$M_{\text{mid}} = \frac{M_{\text{bot}} + M_{\text{top}}}{2} = \frac{1.65 + -1.47}{2} = 0.09 \text{ kNm/m}$$



Slenderness reduction factor

$$e_{top} = \text{MAX}\left(\frac{\text{abs}(1000 * M_{top})}{N_{Ed}} + \frac{h_{ef}}{450}; 0.05 * t_{ef}\right) = 14.47 \text{ mm}$$

$$\Phi_{s,top} = 1 - \frac{2 * e_{top}}{t_{ef}} = 1 - \frac{2 * 14.47}{140.00} = 0.793$$

$$e_{mid} = \text{MAX}\left(\frac{\text{abs}(1000 * M_{mid})}{N_{Ed}} + \frac{h_{ef}}{450}; 0.05 * t_{ef}\right) = 7.00 \text{ mm}$$

$$\Phi_{s,mid} = A_1 * e^{(-0.5 * u^2)} = 0.747$$

$$e_{bot} = \text{MAX}\left(\frac{\text{abs}(1000 * M_{bot})}{N_{Ed}} + \frac{h_{ef}}{450}; 0.05 * t_{ef}\right) = 15.67 \text{ mm}$$

$$\Phi_{s,bot} = 1 - \frac{2 * e_{bot}}{t_{ef}} = 1 - \frac{2 * 15.67}{140.00} = 0.776$$

$$\Phi_s = \text{MIN}(\Phi_{s,top}; \Phi_{s,mid}; \Phi_{s,bot}) = 0.747$$

Material selected

Structural units = Aggregate concrete
 Classification group = 1
 Type of mortar = general

Mean compressive strength of masonry unit $f_b = 7.10 \text{ N/mm}^2$

Compressive strength of mortar $f_m = 6.00 \text{ N/mm}^2$

Shape factor
 Height of unit $h = 215.00 \text{ mm}$
 Width of unit $w = 140.00 \text{ mm}$

$\delta = 1.300$

$f_b = \delta * f_b = 1.300 * 7.10 = 9.23 \text{ N/mm}^2$

$f_k = K * f_b^\alpha * f_m^\beta = 0.55 * 9.23^{0.70} * 6.00^{0.30} = 4.46 \text{ N/mm}^2$

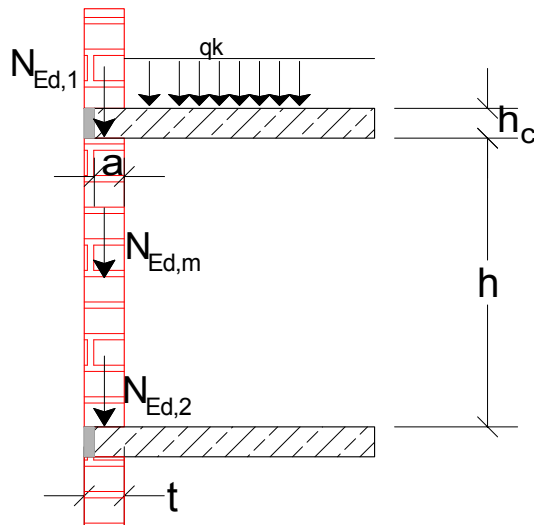
$f_d = \frac{f_k}{\gamma_m} = \frac{4.46}{2.70} = 1.65$

$N_{Rd} = \frac{f_d * t_{ef} * 10^3 * \Phi_A * \Phi_s}{10^3} = \frac{1.65 * 140.00 * 10^3 * 1.00 * 0.747}{10^3} = 172.56 \text{ kN}$

$\frac{N_{Ed}}{N_{Rd}} = \frac{150.00}{172.56} = 0.87 \leq 1$



Load capacity of an external wall



Data given

Effective thickness t_{ef} =	140.00 mm
Clear height h =	2800.00 mm
Effective height reduction factor ρ =	0.75
Total load for ULS N_{Ed} =	150.00 kN/m

Material properties

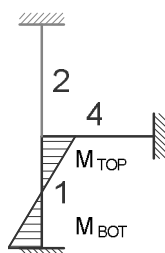
Control class	=	2
Category	=	I
γ_m	=	2.70

Slenderness

Effective height $h_{ef} = \rho * h = 0.75 * 2800.00$	=	2100.00 mm
Slenderness $\lambda = \frac{h_{ef}}{t_{ef}} = \frac{2100.00}{140.00}$	=	15.00 < 27
Factor $\Phi_A =$		1.00



Moments at the top and bottom



Data given for the wall

Clear height $h_1 = h = 2800.00$ mm
 Depth of wall $h = t_{ef} = 140.00$ mm
 Strength $f_k = 4.05$ N/mm²

$E_1 = f_k \cdot 10^3 = 4050.00$ N/mm²

$I_1 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 140.00^3}{12} = 228.67 \cdot 10^6$ mm⁴

Data given for the floor

Load $w_4 = 8.75$ kN/m
 Span $L_4 = 5000.00$ mm
 Floor depth $h = 200.00$ mm

Concrete grade = C30/37

$E_4 = 33000.00$ N/mm²

$I_4 = \frac{850 \cdot h^3}{12} = \frac{850 \cdot 200.00^3}{12} = 566.67 \cdot 10^6$ mm⁴

Moment at the top

$\eta = \frac{E_4 \cdot I_4}{L_4} \cdot \text{MAX} \left(1 - \frac{E_1 \cdot I_1}{4 \cdot \left(\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} \right)} ; 0.5 \right) = 0.50$

$M_{top} = \eta \cdot \frac{E_1 \cdot I_1}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} + \frac{E_4 \cdot I_4}{L_4}} \cdot \frac{-1 \cdot w_4 \cdot L_4^2}{12} = -0.68$ kNm/m

Moment at the bottom

$M_{bot} = \eta \cdot \frac{E_1 \cdot I_1}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} + \frac{E_4 \cdot I_4}{L_4}} \cdot \frac{0.5 \cdot w_4 \cdot L_4^2}{12} = 0.34$ kNm/m

$M_{mid} = \frac{M_{bot} + M_{top}}{2} = \frac{0.34 + -0.68}{2} = -0.17$ kNm/m



Slenderness reduction factor

$$e_{top} = \text{MAX}\left(\frac{\text{abs}(1000 * M_{top})}{N_{Ed}} + \frac{h_{ef}}{450}; 0.05 * t_{ef}\right) = 9.20 \text{ mm}$$

$$\Phi_{s,top} = 1 - \frac{2 * e_{top}}{t_{ef}} = 1 - \frac{2 * 9.20}{140.00} = 0.869$$

$$e_{mid} = \text{MAX}\left(\frac{\text{abs}(1000 * M_{mid})}{N_{Ed}} + \frac{h_{ef}}{450}; 0.05 * t_{ef}\right) = 7.00 \text{ mm}$$

$$\Phi_{s,mid} = A_1 * e^{(-0.5 * u^2)} = 0.747$$

$$e_{bot} = \text{MAX}\left(\frac{\text{abs}(1000 * M_{bot})}{N_{Ed}} + \frac{h_{ef}}{450}; 0.05 * t_{ef}\right) = 7.00 \text{ mm}$$

$$\Phi_{s,bot} = 1 - \frac{2 * e_{bot}}{t_{ef}} = 1 - \frac{2 * 7.00}{140.00} = 0.900$$

$$\Phi_s = \text{MIN}(\Phi_{s,top}; \Phi_{s,mid}; \Phi_{s,bot}) = 0.747$$

Material selected

Structural units = Aggregate concrete
 Classification group = 1
 Type of mortar = general

Mean compressive strength of masonry unit $f_b = 7.10 \text{ N/mm}^2$

Compressive strength of mortar $f_m = 6.00 \text{ N/mm}^2$

Shape factor

Height of unit $h = 215.00 \text{ mm}$

Width of unit $w = 140.00 \text{ mm}$

$\delta = 1.300$

$f_b = \delta * f_b = 1.300 * 7.10 = 9.23 \text{ N/mm}^2$

$f_k = K * f_b^\alpha * f_m^\beta = 0.55 * 9.23^{0.70} * 6.00^{0.30} = 4.46 \text{ N/mm}^2$

$f_d = \frac{f_k}{\gamma_m} = \frac{4.46}{2.70} = 1.65$

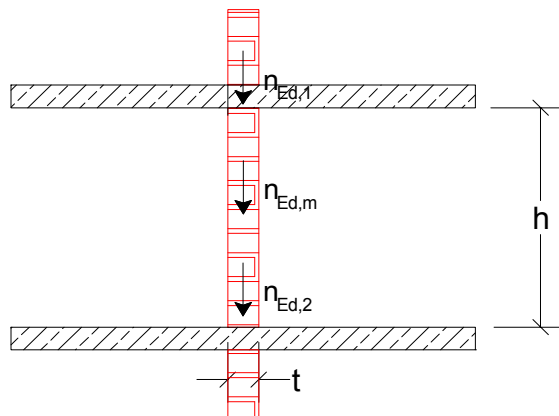
$N_{Rd} = \frac{f_d * t_{ef} * 10^3 * \Phi_A * \Phi_s}{10^3} = \frac{1.65 * 140.00 * 10^3 * 1.00 * 0.747}{10^3} = 172.56 \text{ kN}$

$\frac{N_{Ed}}{N_{Rd}} = \frac{150.00}{172.56} = 0.87 \leq 1$



Chapter 2: Simplified method

Vertical load capacity of an intermediate wall



Data given

Effective thickness t_{ef} =	140.00 mm
Clear height h =	2800.00 mm
Effective height reduction factor ρ =	0.75
Total load for ULS N_{Ed} =	200.00 kN/m

Material properties

Control class	=	2
Category	=	1
γ_m	=	2.70

Reduction factor

Effective height $h_{ef} = \rho * h = 0.75 * 2800.00$	=	2100.00 mm
Slenderness $\lambda = \frac{h_{ef}}{t_{ef}} = \frac{2100.00}{140.00}$	=	15.00 < 27
Factor $\Phi_A =$		1.00
Factor $\Phi_s = 0.85 - 0.0011 * \left(\frac{h_{ef}}{t_{ef}}\right)^2 = 0.85 - 0.0011 * \left(\frac{2100.00}{140.00}\right)^2$	=	0.603

Material selected

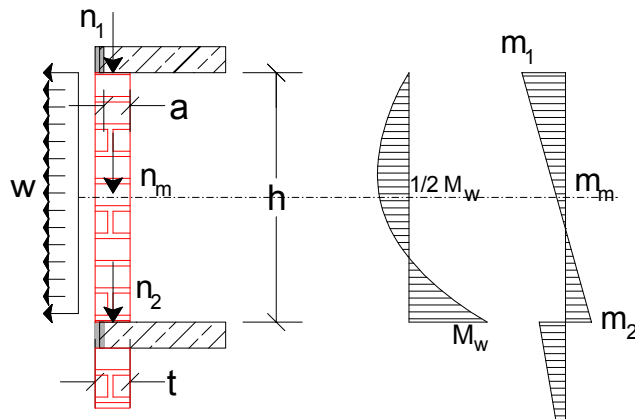
Structural units	=	Aggregate concrete
Classification group	=	1
Type of mortar	=	general
Mean compressive strength of masonry unit $f_b =$	12.00 N/mm ²	
Compressive strength of mortar $f_m =$	6.00 N/mm ²	



$$\begin{aligned} \text{Shape factor} &= & & \\ \text{Height of unit } h &= & 215.00 \text{ mm} & \\ \text{Width of unit } w &= & 140.00 \text{ mm} & \\ \\ \delta &= & 1.300 & \\ \\ f_b &= & \delta * f_b = 1.300 * 12.00 & = & 15.60 \text{ N/mm}^2 & \\ f_k &= & K * f_b^\alpha * f_m^\beta = 0.55 * 15.60^{0.70} * 6.00^{0.30} & = & 6.44 \text{ N/mm}^2 & \\ f_d &= & \frac{f_k}{\gamma_m} = \frac{6.44}{2.70} & = & 2.39 & \\ \\ N_{Rd} &= & \frac{f_d * t_{ef} * 10^3 * \Phi_A * \Phi_s}{10^3} = \frac{2.39 * 140.00 * 10^3 * 1.00 * 0.603}{10^3} & = & 201.76 \text{ kN/m} & \\ \\ \frac{N_{Ed}}{N_{Rd}} &= & \frac{200.00}{201.76} & = & \mathbf{0.99} \leq \mathbf{1} & \end{aligned}$$



Load capacity of an external wall (roof)



Data given

Effective thickness t_{ef} =	140.00 mm
Clear height h =	2800.00 mm
Span of roof $l_{f,ef}$ =	5000.00 mm
Effective height reduction factor ρ =	1.00

Loading

Dead loads g_k =	15.00 kN/m
Imposed loads q_k =	10.00 kN/m
Windload q_{Ewd} =	0.60 kN/m ²

Ultimate limit states

$$\text{Total load for ULS } N_{Ed} = 1.35 * g_k + 1.50 * q_k = 35.25 \text{ kN/m}$$

Material properties

Control class	=	2
Category	=	I
γ_m	=	2.70

Slenderness

Effective height $h_{ef} = \rho * h$	=	1.00 * 2800.00	=	2800.00 mm
Slenderness $\lambda = \frac{h_{ef}}{t_{ef}}$	=	$\frac{2800.00}{140.00}$	=	20.00 < 27
Factor Φ_A	=		=	1.00
Factor $\Phi_{s,i} = 0.85 - 0.0011 * \left(\frac{h_{ef}}{t_{ef}}\right)^2$	=	$0.85 - 0.0011 * \left(\frac{2800.00}{140.00}\right)^2$	=	0.410
Factor $\Phi_{s,ii} = 1.3 - \frac{l_{f,ef}}{8}$	=	$1.3 - \frac{5.00}{8}$	=	0.675
Factor $\Phi_{s,iii}$	=		=	0.400
$\Phi_s = \text{MIN}(\Phi_{s,i}; \Phi_{s,ii}; \Phi_{s,iii})$	=		=	0.40



Material selected

Structural units = Aggregate concrete
Classification group = 1
Type of mortar = general

Mean compressive strength of masonry unit $f_b = 12.00 \text{ N/mm}^2$
Compressive strength of mortar $f_m = 6.00 \text{ N/mm}^2$

Shape factor
Height of unit $h = 215.00 \text{ mm}$
Width of unit $w = 140.00 \text{ mm}$

$\delta = 1.300$

$f_b = \delta * f_b = 1.300 * 12.00 = 15.60 \text{ N/mm}^2$

$f_k = K * f_b^\alpha * f_m^\beta = 0.55 * 15.60^{0.70} * 6.00^{0.30} = 6.44 \text{ N/mm}^2$

$f_d = \frac{f_k}{\gamma_m} = \frac{6.44}{2.70} = 2.39$

$N_{Rd} = \frac{f_d * t_{ef} * 10^3 * \Phi_A * \Phi_S}{10^3} = \frac{2.39 * 140.00 * 10^3 * 1.00 * 0.40}{10^3} = 133.84 \text{ kN}$

$\frac{N_{Ed}}{N_{Rd}} = \frac{35.25}{133.84} = 0.26 \leq 1$

Minimum thickness

$N_{Ed} = g_k = 15.00 \text{ kN/m}$

$\alpha = \frac{N_{Ed}}{t_{ef} * 1000 * f_d} = \frac{15000}{140.00 * 1000 * 2.39} = 0.04 \text{ m}^{-1}$

$c_1 = 0.120$

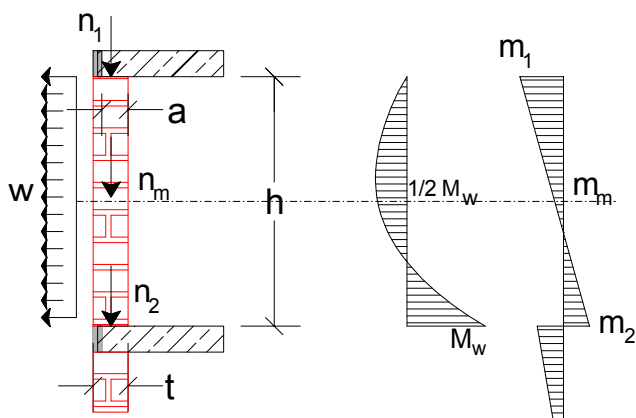
$c_2 = 0.017$

$t_{min} = \frac{c_1 * q_{Ewd} * 1 * h_{ef}^2}{N_{Ed}} + c_2 * h_{ef} = \frac{0.120 * 0.60 * 1 * 2.80^2}{15.00} + 0.017 * 2.80 = 0.085 \text{ m}$

$\frac{t_{min}}{t_{ef}} = \frac{85}{140.00} = 0.61 \leq 1$



Load capacity of an external wall



Data given

Effective thickness t_{ef} =	140.00 mm
Clear height h =	2800.00 mm
Span of floor $l_{f,ef}$ =	5000.00 mm
Effective height reduction factor ρ =	1.00

Loading

Dead loads g_k =	50.00 kN/m
Imposed loads q_k =	30.00 kN/m
Windload q_{Ewd} =	0.60 kN/m ²

Ultimate limit states

$$\text{Total load for ULS } N_{Ed} = 1.35 * g_k + 1.50 * q_k = 112.50 \text{ kN/m}$$

Material properties

Control class	=	2
Category	=	I
γ_m	=	2.70

Slenderness

$$\text{Effective height } h_{ef} = \rho * h = 1.00 * 2800.00 = 2800.00 \text{ mm}$$

$$\text{Slenderness } \lambda = \frac{h_{ef}}{t_{ef}} = \frac{2800.00}{140.00} = 20.00 < 27$$

$$\text{Factor } \Phi_A = 1.00$$

$$\text{Factor } \Phi_{s,i} = 0.85 - 0.0011 * \left(\frac{h_{ef}}{t_{ef}} \right)^2 = 0.85 - 0.0011 * \left(\frac{2800.00}{140.00} \right)^2 = 0.410$$

$$\text{Factor } \Phi_{s,ii} = 1.3 - \frac{l_{f,ef}}{8} = 1.3 - \frac{5.00}{8} = 0.675$$

$$\Phi_s = \text{MIN}(\Phi_{s,i}; \Phi_{s,ii}) = 0.41$$



Material selected

Structural units = Aggregate concrete
 Classification group = 1
 Type of mortar = general

Mean compressive strength of masonry unit $f_b = 12.00 \text{ N/mm}^2$
 Compressive strength of mortar $f_m = 6.00 \text{ N/mm}^2$

Shape factor
 Height of unit $h = 215.00 \text{ mm}$
 Width of unit $w = 140.00 \text{ mm}$

$\delta = 1.300$

$f_b = \delta * f_b = 1.300 * 12.00 = 15.60 \text{ N/mm}^2$

$f_k = K * f_b^\alpha * f_m^\beta = 0.55 * 15.60^{0.70} * 6.00^{0.30} = 6.44 \text{ N/mm}^2$

$f_d = \frac{f_k}{\gamma_m} = \frac{6.44}{2.70} = 2.39$

$N_{Rd} = \frac{f_d * t_{ef} * 10^3 * \Phi_A * \Phi_S}{10^3} = \frac{2.39 * 140.00 * 10^3 * 1.00 * 0.41}{10^3} = 137.19 \text{ kN}$

$\frac{N_{Ed}}{N_{Rd}} = \frac{112.50}{137.19} = 0.82 \leq 1$

Minimum thickness

$N_{Ed} = g_k = 50.00 \text{ kN/m}$

$\alpha = \frac{N_{Ed}}{t_{ef} * 1000 * f_d} = \frac{50000}{140.00 * 1000 * 2.39} = 0.15 \text{ m}^{-1}$

$c_1 = 0.1300$

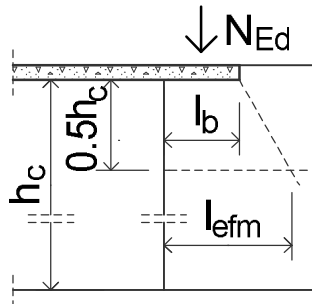
$c_2 = 0.0205$

$t_{min} = \frac{c_1 * q_{Ewd} * 1 * h_{ef}^2}{N_{Ed}} + c_2 * h_{ef} = \frac{0.1300 * 0.60 * 1 * 2.80^2}{50.00} + 0.0205 * 2.80 = 0.070 \text{ m}$

$\frac{t_{min}}{t_{ef}} = \frac{70}{140.00} = 0.50 \leq 1$

Chapter 3: Concentrated loads

Lintel bearing



Data given

Clear Height h =	2800.0 mm
Height of lintel h_{beam} =	200.0 mm
Distance to the nearest edge a_1 =	0.0 mm
Length of bearing l_b =	425.0 mm
Wall thickness t =	140.0 mm
Single load N_{Ed} =	100.00 kN
Load from floor and above q_d =	75.00 kN/m

Material properties

Mean compressive strength of masonry unit f_b =	12.00 N/mm ²
Characteristic self-weight of units g_{unit} =	2.70 kN/m ²
Compressive strength of mortar f_m =	6.00 N/mm ²
Structural units	= Aggregate concrete
Classification group	= 1
Type of mortar	= general
Control class	= 2
Category	= II
γ_m	= 3.00

Capacity of bearing area under the load

$\text{max.}f$ =	IF(group = "1" ; 1.5 ; 1.00)	=	1.50
Required $f_{b,\text{requ}}$ =	$\text{MAX}\left(\frac{N_{\text{Ed}}}{1.2 \cdot l_b \cdot t}; \frac{N_{\text{Ed}}}{\text{max.}f \cdot l_b \cdot t}\right)$	=	1.40 N/mm ²

At this level the load is carried on a length l_{efm} of wall

h_c =	$h - h_{\text{beam}} = 2800.0 - 200.0$	=	2600.0 mm
Length l_{efm} =	$l_b + \frac{0.5 \cdot h_c}{\tan(60)} = 425.0 + \frac{0.5 \cdot 2600.0}{\tan(60)}$	=	1175.56 mm
Weight of Wall N_{wall} =	$1.35 \cdot g_{\text{unit}} \cdot \left(\frac{h_c}{2} + h_{\text{beam}}\right) \cdot l_{\text{efm}}$		
	$= 1.35 \cdot 2.70 \cdot \left(\frac{2.6}{2} + 0.2\right) \cdot 1.17556$	=	6.43 kN
From above N_{above} =	$q_d \cdot (l_{\text{efm}} - l_b) = 75.00 \cdot (1.17556 - 0.425)$	=	56.29 kN
Ultimate design load F =	$N_{\text{Ed}} + N_{\text{wall}} + N_{\text{above}} = 100.00 + 6.43 + 56.29$	=	162.72 kN



Reduction factor

$$\text{Effective height } h_{ef} = 0.75 * h = 0.75 * 2800.0 = 2100.00 \text{ mm}$$

$$\text{Slenderness } \lambda = \frac{h_{ef}}{t} = \frac{2100.00}{140.0} = 15.00 < 27$$

$$\text{Factor } \Phi_A = 1.00$$

$$\text{Factor } \Phi_s = 0.85 - 0.0011 * \left(\frac{h_{ef}}{t}\right)^2 = 0.85 - 0.0011 * \left(\frac{2100.00}{140.0}\right)^2 = 0.603$$

Required f_d and f_k

$$\sigma = \frac{F}{l_{efm} * t} = \frac{162720}{1175.56 * 140.0} = 0.99 \text{ N/mm}^2$$

$$\text{Required value } f_{d,requ} = \frac{\sigma}{\Phi_A * \Phi_s} = \frac{0.99}{1.00 * 0.603} = 1.64 \text{ N/mm}^2$$

$$\text{Required value } f_{k,requ} = f_{d,requ} * \gamma_m = 1.64 * 3.00 = 4.92 \text{ N/mm}^2$$

Units selected

$$\begin{aligned} \text{Shape factor} & \\ \text{Height of unit } h & = 215.00 \text{ mm} \\ \text{Width of unit } w & = 140.00 \text{ mm} \end{aligned}$$

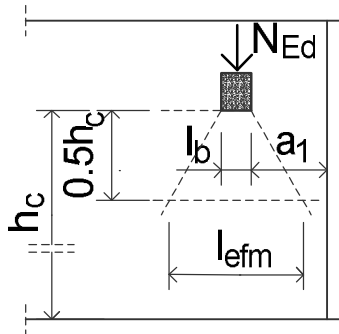
$$\delta = 1.300$$
$$f_b = \delta * f_b = 1.300 * 12.00 = 15.60 \text{ N/mm}^2$$

$$f_k = K * f_b^\alpha * f_m^\beta = 0.55 * 15.60^{0.70} * 6.00^{0.30} = 6.44 \text{ N/mm}^2$$

$$\frac{f_{k,requ}}{f_k} = \frac{4.92}{6.44} = 0.76 \leq 1$$



Beam bearing on a wall



Data given

Clear Height $h =$	2800.0 mm
Span of floor $l_{f,ef} =$	5000.0 mm
Width of beam $b_{beam} =$	200.0 mm
Height of beam $h_{beam} =$	300.0 mm
Distance to the nearest edge $a_1 =$	2000.0 mm
Wall thickness $t =$	140.0 mm
Single load $N_{Ed} =$	100.00 kN
Load from floor and above $q_d =$	30.00 kN/m

Material properties

Mean compressive strength of masonry unit $f_b =$	12.00 N/mm ²
Characteristic self-weight of units $g_{unit} =$	3.00 kN/m ²
Compressive strength of mortar $f_m =$	6.00 N/mm ²

Structural units	= Aggregate concrete
Classification group	= 1
Type of mortar	= general
Control class	= 2
Category	= 1

γ_m	= 2.70
------------	--------

Capacity of bearing area under the load

$$h_c = h - h_{beam} = 2800.0 - 300.0 = 2500.0 \text{ mm}$$

$$\text{max.f} = \text{IF}(\text{group} = "1"; 1.5; 1.00) = 1.50$$

$$\text{Design load } N = N_{Ed} + q_d * b_{beam} = 100.00 + 30.00 * 0.2 = 106.00 \text{ kN}$$

$$\text{Required } f_{b,requ} = \text{MAX}\left(\frac{N}{\left(1.2 + \frac{0.4 * a_1}{h_c}\right) * b_{beam} * t}; \frac{N}{\text{max.f} * b_{beam} * t}\right) = 2.52 \text{ N/mm}^2$$



At this level the load is carried on a length l_{efm} of wall

$$\text{Length } l_{efm} = b_{\text{beam}} + \frac{h_c}{\tan(60)} = 200.0 + \frac{2500.0}{\tan(60)} = 1643.38 \text{ mm}$$

$$\begin{aligned} \text{Weight of Wall } N_{\text{wall}} &= 1.35 * g_{\text{unit}} * \left(\frac{h_c}{2} + h_{\text{beam}} \right) * l_{efm} \\ &= 1.35 * 3.00 * \left(\frac{2.5}{2} + 0.3 \right) * 1.64338 = 10.32 \text{ kN} \end{aligned}$$

$$\text{From above } N_{\text{above}} = q_d * l_{efm} = 30.00 * 1.64338 = 49.30 \text{ kN}$$

$$\text{Ultimate design load } F = N_{Ed} + N_{\text{wall}} + N_{\text{above}} = 100.00 + 10.32 + 49.30 = 159.62 \text{ kN}$$

Reduction factor

$$\text{Effective height } h_{ef} = 1.00 * h = 1.00 * 2800.0 = 2800.00 \text{ mm}$$

$$\text{Slenderness } \lambda = \frac{h_{ef}}{t} = \frac{2800.00}{140.0} = 20.00 < 27$$

$$\text{Factor } \Phi_A = 1.00$$

$$\text{Factor } \Phi_{s,i} = 0.85 - 0.0011 * \left(\frac{h_{ef}}{t} \right)^2 = 0.85 - 0.0011 * \left(\frac{2800.00}{140.0} \right)^2 = 0.410$$

$$\text{Factor } \Phi_{s,ii} = 1.3 - \frac{l_{f,ef}}{8} = 1.3 - \frac{5.0}{8} = 0.675$$

$$\text{Factor } \Phi_{s,iii} = 0.400$$

$$\Phi_s = \text{MIN}(\Phi_{s,i}; \Phi_{s,ii}; \Phi_{s,iii}) = 0.400$$

Required f_d and f_k

$$\sigma = \frac{F}{l_{efm} * t} = \frac{159620}{1643.38 * 140.0} = 0.69 \text{ N/mm}^2$$

$$\text{Required value } f_{d,requ} = \frac{\sigma}{\Phi_A * \Phi_s} = \frac{0.69}{1.00 * 0.400} = 1.73 \text{ N/mm}^2$$

$$\text{Required value } f_{k,requ} = f_{d,requ} * \gamma_m = 1.73 * 2.70 = 4.67 \text{ N/mm}^2$$

Units selected

$$\begin{aligned} \text{Shape factor } \delta &= 1.300 \\ \text{Height of unit } h &= 215.00 \text{ mm} \\ \text{Width of unit } w &= 140.00 \text{ mm} \end{aligned}$$

$$\begin{aligned} f_b &= \delta * f_b = 1.300 * 12.00 = 15.60 \text{ N/mm}^2 \end{aligned}$$

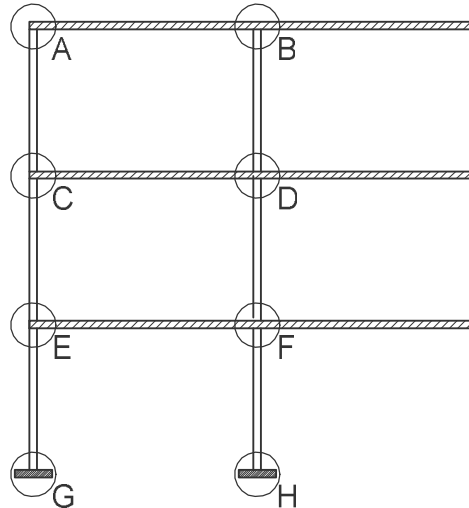
$$f_k = K * f_b^\alpha * f_m^\beta = 0.55 * 15.60^{0.70} * 6.00^{0.30} = 6.44 \text{ N/mm}^2$$

$$\frac{f_{k,requ}}{f_k} = \frac{4.67}{6.44} = 0.73 \leq 1$$

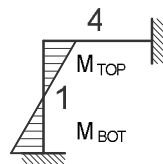


Chapter 4: Formulas for moments

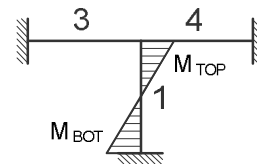
Content: Formulae for the moment of a wall panel



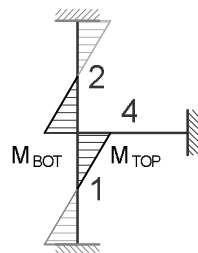
Overview



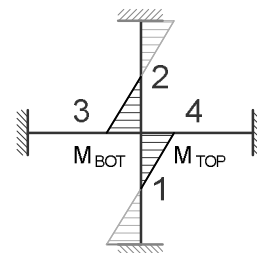
load



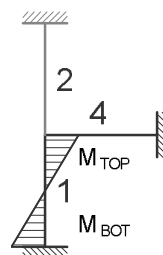
load



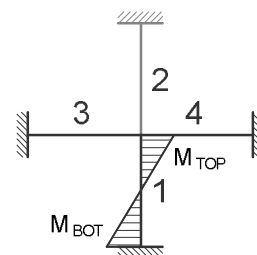
load



load



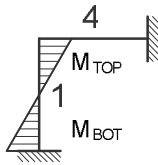
load



load



Formula for the moment of a wall panel (A)



Data given for the wall

Clear height $h_1 = 2800.00$ mm
 Depth of wall $h = 215.00$ mm
 Strength $f_k = 4.05$ N/mm²

$$E_1 = f_k \cdot 10^3 = 4050.00 \text{ N/mm}^2$$

$$I_1 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 215.00^3}{12} = 828.20 \cdot 10^6 \text{ mm}^4$$

Data given for the roof

Load $w_4 = 10.00$ kN/m
 Span of roof $L_4 = 5000.00$ mm
 Roof or floor depth $h = 200.00$ mm

Concrete grade = C30/37

$$E_4 = 33000.00 \text{ N/mm}^2$$

$$I_4 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 200.00^3}{12} = 666.67 \cdot 10^6 \text{ mm}^4$$

Moment at the top

$$\eta = \text{MAX} \left(1 - \frac{\frac{E_4 \cdot I_4}{L_4}}{4 \cdot \frac{E_1 \cdot I_1}{h_1}}; 0.5 \right) = 0.50$$

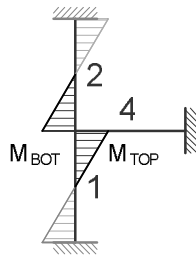
$$M_{\text{TOP}} = \eta \cdot \frac{\frac{E_1 \cdot I_1}{h_1} + \frac{E_4 \cdot I_4}{L_4}}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_4 \cdot I_4}{L_4}} \cdot \frac{-1 \cdot w_4 \cdot L_4^2}{12} = -2.23 \text{ kNm/m}$$

Moment at the bottom

$$M_{\text{BOT}} = \eta \cdot \frac{\frac{E_1 \cdot I_1}{h_1} + \frac{E_4 \cdot I_4}{L_4}}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_4 \cdot I_4}{L_4}} \cdot \frac{w_4 \cdot L_4^2}{12} \cdot 0.5 = 1.11 \text{ kNm/m}$$



Formula for the moment of a wall panel (C)



Data given for the wall

Clear height $h_1 = 2500.00$ mm
 Clear height $h_2 = 2500.00$ mm
 Depth of wall $h = 215.00$ mm
 Strength $f_k = 4.05$ N/mm²

$$E_1 = f_k \cdot 10^3 = 4050.00 \text{ N/mm}^2$$

$$I_1 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 215.00^3}{12} = 828.20 \cdot 10^6 \text{ mm}^4$$

Parameter of the wall 2 are the same as wall 1: $E_1 = E_2$ and $I_1 = I_2$

Data given for the floor

Load $w_4 = 7.50$ kN/m
 Span of floor $L_4 = 5000.00$ mm
 Floor depth $h = 200.00$ mm

Concrete grade = C30/37

$$E_4 = 33000.00 \text{ N/mm}^2$$

$$I_4 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 200.00^3}{12} = 666.67 \cdot 10^6 \text{ mm}^4$$

Moment at the bottom

$$\eta = \frac{E_4 \cdot I_4}{L_4} \cdot \text{MAX}\left(1 - \frac{1}{4 \cdot \left(\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2}\right)}; 0.5\right) = 0.59$$

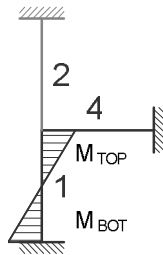
$$M_{\text{BOT}} = \eta \cdot \frac{E_1 \cdot I_1}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} + \frac{E_4 \cdot I_4}{L_4}} \cdot \frac{w_4 \cdot L_4^2}{12} = 1.75 \text{ kNm/m}$$

Moment at the top

$$M_{\text{TOP}} = \eta \cdot \frac{E_1 \cdot I_1}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} + \frac{E_4 \cdot I_4}{L_4}} \cdot \frac{-1 \cdot w_4 \cdot L_4^2}{12} = -1.75 \text{ kNm/m}$$



Formula for the moment of a wall panel (E)



Data given for the wall

Clear height $h_1 = 2500.00$ mm
 Clear height $h_2 = 2500.00$ mm
 Depth of wall $h = 215.00$ mm
 Strength $f_k = 4.05$ N/mm²

$$E_1 = f_k \cdot 10^3 = 4050.00 \text{ N/mm}^2$$

$$I_1 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 215.00^3}{12} = 828.20 \cdot 10^6 \text{ mm}^4$$

Parameter of the wall 2 are the same as wall 1: $E_1 = E_2$ and $I_1 = I_2$

Data given for the floor

Load $w_4 = 7.50$ kN/m
 Span of floor $L_4 = 5000.00$ mm
 Floor depth $h = 200.00$ mm

Concrete grade = C30/37

$$E_4 = 33000.00 \text{ N/mm}^2$$

$$I_4 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 200.00^3}{12} = 666.67 \cdot 10^6 \text{ mm}^4$$

Moment at the top

$$\eta = \frac{E_4 \cdot I_4}{L_4} \cdot \text{MAX} \left(1 - \frac{1}{4 \cdot \left(\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} \right)}; 0.5 \right) = 0.59$$

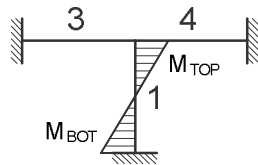
$$M_{TOP} = \eta \cdot \frac{\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} + \frac{E_4 \cdot I_4}{L_4}}{12} \cdot (-1 \cdot w_4 \cdot L_4^2) = -1.75 \text{ kNm/m}$$

Moment at the bottom

$$M_{BOT} = \eta \cdot \frac{\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} + \frac{E_4 \cdot I_4}{L_4}}{12} \cdot (0.5 \cdot w_4 \cdot L_4^2) = 0.87 \text{ kNm/m}$$



Formula for the moment of a wall panel (B)



Data given for the wall

Clear height $h_1 = 2500.00$ mm
 Depth of wall $h = 215.00$ mm
 Strength $f_k = 4.05$ N/mm²

$$E_1 = f_k \cdot 10^3 = 4050.00 \text{ N/mm}^2$$

$$I_1 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 215.00^3}{12} = 828.20 \cdot 10^6 \text{ mm}^4$$

Data given for the floor or roof

Load $w_3 = 3.75$ kN/m
 Load $w_4 = 7.50$ kN/m
 Span of floor $L_3 = 5000.00$ mm
 Span of floor $L_4 = 5000.00$ mm
 Floor depth $h = 200.00$ mm

Concrete grade = C30/37
 $E_3 = 33000.00$ N/mm²

$$I_3 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 200.00^3}{12} = 666.67 \cdot 10^6 \text{ mm}^4$$

Parameter of the floor 4 are the same as wall 3: $E_4 = E_3$ and $I_4 = I_3$

Moment at the top

$$\eta = \text{MAX} \left(1 - \frac{\frac{E_3 \cdot I_3}{L_3} + \frac{E_4 \cdot I_4}{L_4}}{4 \cdot \left(\frac{E_1 \cdot I_1}{h_1} \right)}; 0.5 \right) = 0.50$$

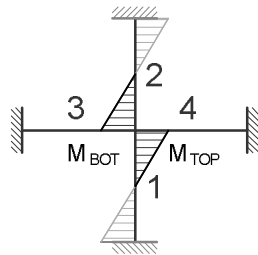
$$M_{\text{TOP}} = \frac{E_1 \cdot I_1}{h_1} \cdot \frac{\eta}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_3 \cdot I_3}{L_3} + \frac{E_4 \cdot I_4}{L_4}} \cdot \left(\frac{w_3 \cdot L_3^2}{12} - \frac{w_4 \cdot L_4^2}{12} \right) = -0.52 \text{ kNm/m}$$

Moment at the bottom

$$M_{\text{BOT}} = \frac{E_1 \cdot I_1}{h_1} \cdot \frac{\eta}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_3 \cdot I_3}{L_3} + \frac{E_4 \cdot I_4}{L_4}} \cdot \left(\frac{w_4 \cdot L_4^2}{12} - \frac{w_3 \cdot L_3^2}{12} \right) \cdot 0.5 = 0.26 \text{ kNm/m}$$



Formula for the moment of a wall panel (D)



Data given for the wall

Clear height h_1 =	2500.00 mm
Clear height h_2 =	2500.00 mm
Depth of wall h =	215.00 mm
Strength f_k =	4.05 N/mm ²

$$E_1 = f_k \cdot 10^3 = 4050.00 \text{ N/mm}^2$$

$$I_1 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 215.00^3}{12} = 828.20 \cdot 10^6 \text{ mm}^4$$

Parameter of the wall 2 are the same as wall 1: $E_1 = E_2$ and $I_1 = I_2$

Data given for the floor

Load w_3 =	2.50 kN/m
Load w_4 =	7.50 kN/m
Span of floor L_3 =	5000.00 mm
Span of floor L_4 =	5000.00 mm
Floor depth h =	200.00 mm

Concrete grade = C30/37

$$E_3 = 33000.00 \text{ N/mm}^2$$

$$I_3 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 200.00^3}{12} = 666.67 \cdot 10^6 \text{ mm}^4$$

Parameter of the floor 4 are the same as wall 3: $E_4 = E_3$ and $I_4 = I_3$

Moment at the bottom

$$\eta = \text{MAX} \left(1 - \frac{\frac{E_3 \cdot I_3}{L_3} + \frac{E_4 \cdot I_4}{L_4}}{4 \cdot \left(\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} \right)} ; 0.5 \right) = 0.50$$

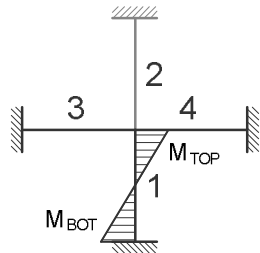
$$M_{\text{BOT}} = \eta \cdot \frac{\frac{E_1 \cdot I_1}{h_1}}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} + \frac{E_3 \cdot I_3}{L_3} + \frac{E_4 \cdot I_4}{L_4}} \cdot \left(\frac{w_4 \cdot L_4^2}{12} - \frac{w_3 \cdot L_3^2}{12} \right) = 0.61 \text{ kNm/m}$$

Moment at the top

$$M_{\text{TOP}} = \eta \cdot \frac{\frac{E_1 \cdot I_1}{h_1}}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} + \frac{E_3 \cdot I_3}{L_3} + \frac{E_4 \cdot I_4}{L_4}} \cdot \left(\frac{w_3 \cdot L_3^2}{12} - \frac{w_4 \cdot L_4^2}{12} \right) = -0.61 \text{ kNm/m}$$



Formula for the moment of a wall panel (F)



Data given for the wall

Clear height $h_1 =$	2500.00 mm
Clear height $h_2 =$	2500.00 mm
Depth of wall $h =$	215.00 mm
Strength $f_k =$	4.05 N/mm ²

$$E_1 = f_k \cdot 10^3 = 4050.00 \text{ N/mm}^2$$

$$I_1 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 215.00^3}{12} = 828.20 \cdot 10^6 \text{ mm}^4$$

Parameter of the wall 2 are the same as wall 1: $E_1 = E_2$ and $I_1 = I_2$

Data given for the floor

Load $w_3 =$	2.50 kN/m
Load $w_4 =$	7.50 kN/m
Span of floor $L_3 =$	5000.00 mm
Span of floor $L_4 =$	5000.00 mm
Floor depth $h =$	200.00 mm

$$\text{Concrete grade} = \text{C30/37}$$

$$E_3 = 33000.00 \text{ N/mm}^2$$

$$I_3 = \frac{1000 \cdot h^3}{12} = \frac{1000 \cdot 200.00^3}{12} = 666.67 \cdot 10^6 \text{ mm}^4$$

Parameter of the floor 4 are the same as wall 3: $E_4 = E_3$ and $I_4 = I_3$

Moment at the top

$$\eta = \text{MAX} \left(1 - \frac{\frac{E_3 \cdot I_3}{L_3} + \frac{E_4 \cdot I_4}{L_4}}{4 \cdot \left(\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} \right)} ; 0.5 \right) = 0.50$$

$$M_{\text{TOP}} = \eta \cdot \frac{\frac{E_1 \cdot I_1}{h_1}}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} + \frac{E_3 \cdot I_3}{L_3} + \frac{E_4 \cdot I_4}{L_4}} \cdot \left(\frac{w_3 \cdot L_3^2}{12} - \frac{w_4 \cdot L_4^2}{12} \right) = -0.61 \text{ kNm/m}$$

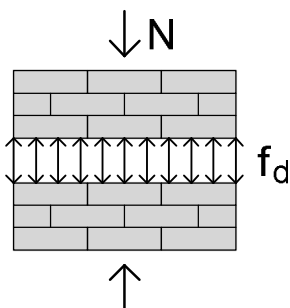
Moment at the bottom

$$M_{\text{BOT}} = \eta \cdot \frac{\frac{E_1 \cdot I_1}{h_1}}{\frac{E_1 \cdot I_1}{h_1} + \frac{E_2 \cdot I_2}{h_2} + \frac{E_3 \cdot I_3}{L_3} + \frac{E_4 \cdot I_4}{L_4}} \cdot \left(\frac{w_4 \cdot L_4^2}{12} - \frac{w_3 \cdot L_3^2}{12} \right) \cdot 0.5 = 0.30 \text{ kNm/m}$$



Chapter 5: Material

Compressive strength of masonry



Material properties

Structural units	=	Clay
Classification group	=	1
Type of mortar	=	general

Mean compressive strength of masonry unit f_b	=	12.00 N/mm ²
Compressive strength of mortar f_m	=	6.00 N/mm ²

Values of constants

K	=	0.50
α	=	0.70
β	=	0.30

Shape factor

Height of unit h	=	65.00 mm
Width of unit w	=	102.50 mm
δ	=	0.845
f_b	$\delta * f_b = 0.845 * 12.00$	= 10.14 N/mm ²

Compressive strength

Characteristic compressive strength		
f_k	$K * f_b^\alpha * f_m^\beta = 0.50 * 10.14^{0.70} * 6.00^{0.30}$	= 4.33 N/mm ²

Control class	=	2
Category	=	1

γ_m	=	2.70
------------	---	------

Design compressive strength

f_d	$\frac{f_k}{\gamma_m} = \frac{4.33}{2.70}$	= 1.60
-------	--	--------